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CERTIFICATION

I, the below named translator, hereby declare that: my name and post office address are as stated below; that I am knowledgeable in the English and German languages, and that I believe that the attached text is a true and complete translation of PCT/DE2004/002455, filed with the German Patent Office on November 2, 2004.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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1 Description

2

3 Switching device

4

5 The invention relates to a switching device having a first
6 and a second arcing contact piece, which lie axially
7 opposite one another, and a first and a second rated current
8 contact piece, which are arranged coaxially with respect to
9 the arcing contact pieces, at least one of the rated current
10 contact pieces having a hollow-cylindrical basic body, which
11 is covered at the front by an arc-resistant material at its
12 end facing a switching path of the switching device.

13

14 Such a switching device has been disclosed, for example, in
15 the European patent application EP 0 982 748 A1. Therein,
16 the arcing contact pieces are covered by an arc-resistant
17 material by means of plasma spraying such that an arc drawn
18 between the arcing contact pieces does not cause any
19 erosion, or only causes a very low amount of erosion.
20 Furthermore, the rated current contact pieces likewise have
21 an erosion-resistant protective coating, which is applied by
22 means of plasma spraying, in sections on their sliding
23 faces. The stationary rated current contact piece is silver-
24 plated on top of the erosion-resistant protective coating.

25

26 When two or more materials, such as the erosion-resistant
27 material, the electrically conductive silver and a further
28 metal such as the aluminum of the rated current contact
29 piece, impact against one another, the respective points of
30 impact always have irregularities. The point of impact can
31 only be subjected to a mechanical load to a reduced extent.
32 Surface friction occurring in the event of the sliding faces
33 of the rated current contact pieces running against one
34 another can result in disintegration phenomena and thus in a
35 weakening of the individual layers. It is thus possible for

1 individual layers to be chipped off starting from the point
2 of impact. This reduces the switching capacity of the
3 switching device.

4
5 The invention is based on the object of designing a
6 switching device of the type mentioned initially such that
7 the contact points withstand high mechanical and thermal
8 loads while having a high current-carrying capacity.

9
10 The object is achieved according to the invention in the
11 case of the switching device of the type mentioned initially
12 by the fact that the arc-resistant material has an
13 electroplating.

14
15 The electroplating may consist, for example, of an
16 electrically highly conductive material, such as silver or
17 gold. This reduces the contact resistance of the electrical
18 contact. At the same time, the electroplating prevents
19 oxidation on the arc-resistant material in the event that
20 the individual components are stored for a relatively long
21 period of time. By including the arc-resistant material in
22 an electroplating treatment process, it is possible to cover
23 points of impact or boundary layers of different materials,
24 which improves the mechanical loadability and the mechanical
25 endurance of these points.

26
27 One advantageous refinement can furthermore provide for the
28 arc-resistant material to be fixed to the hollow-cylindrical
29 basic body in the form of a ring, so as to cover front faces
30 of the hollow-cylindrical basic body.

31 Owing to the fact that the front faces of the hollow-
32 cylindrical basic body are covered, the electric field in
33 the direction of the switching path of the switching device
34 is substantially controlled by the form of the ring. This
35 results in the possibility of using manufacturing methods

1 for manufacturing the basic body with a lesser degree of
2 precision, for example a reduced surface quality, than in
3 the case of the ring used for field control. Furthermore, it
4 is possible to equip the basic body with various ring forms
5 so as to achieve various electric field effects in the
6 region of the switching path of the switching device.
7 Furthermore, when the front faces of the hollow-cylindrical
8 basic body are completely covered, the basic body itself is
9 protected against the effect of a switching arc. It is thus
10 possible for an arc to act on many points on the ring. The
11 stability of the ring is thus increased. Splitting into a
12 hollow-cylindrical basic body and a ring also furthermore
13 has the advantage that the hollow-cylindrical basic body can
14 be produced, for example, from a material having a low
15 density, such as aluminum, as a result of which the total
16 mass of the hollow-cylindrical basic body and the arc-
17 resistant material fixed thereto is reduced. Arc-resistant
18 materials are, for example, mixtures of molybdenum (Mo),
19 tungsten (W), copper (Cu) and silver (Ag). For example,
20 CuCrZr, CuZn39Pb3 or Ecu57 can be used for the arc-resistant
21 material. These materials have a very high density, which
22 results in the ring having a comparatively high mass. In
23 particular in the event of a movement of the rated current
24 contact piece equipped with the arc-resistant material, the
25 multi-part design of the rated current contact piece limits
26 the mass to be moved.

27
28 Provision may advantageously further be made for the ring to
29 have a smaller radial wall thickness at its end facing away
30 from the switching path than at its end facing the switching
31 path.

32
33 Owing to the high density which has already been mentioned
34 above, even small components consisting of an arc-resistant
35 material have a comparatively high mass. A reduction in the

1 wall thicknesses to the absolute minimum required therefore
2 makes it possible to make savings on the arc-resistant
3 material. Furthermore, in the case of a stepped design of
4 the ring, in which the end facing the switching path has a
5 greater wall thickness than the end facing away from the
6 switching path, it is possible for the ring to be pushed
7 onto the hollow-cylindrical basic body in a simple manner.
8 Owing to this design for the form of the ring, it can be
9 pushed onto the hollow-cylindrical basic body automatically
10 in a centering manner. This simplifies assembly. At the same
11 time, the points of the hollow-cylindrical basic body and
12 the arc-resistant ring which are coming into contact with
13 one another are increased in number owing to the enlarged
14 area. Owing to an increased number of contact points, the
15 electrical contact resistance between the arc-resistant ring
16 and the hollow-cylindrical basic body is reduced.

17
18 One further advantageous refinement may provide for the ring
19 to be pressed against the hollow-cylindrical basic body of
20 the rated current contact piece in the axial direction by
21 means of a bolt connection.

22
23 A bolt connection in the axial direction between the ring
24 and the hollow-cylindrical basic body makes it possible to
25 keep the outer contours of the ring and the hollow-
26 cylindrical basic body free from drilled holes or other
27 fixing means. The outer contour of the rated current contact
28 piece is thus maintained. Furthermore, owing to an
29 arrangement of the bolt connections in the axial direction
30 in the interior of the hollow-cylindrical basic body, a
31 sufficient volume remains free for accommodating, for
32 example, further assemblies or for deflecting or guiding the
33 quenching gas flows occurring in the event of a switching
34 operation in the interior. Threaded rods, screws, pressed or
35 crimped bolts or bolts which have been adhesively bonded-in

1 etc. can be used for bolting purposes. In this case, the
2 bolts form a type of cage with their longitudinal axes
3 parallel to the cylinder axis of the hollow-cylindrical
4 basic body. Owing to an even distribution over the
5 circumference of the hollow-cylindrical basic body, the ring
6 can be pressed uniformly against the hollow-cylindrical
7 basic body.

8
9 One further advantageous refinement may provide for the
10 hollow-cylindrical basic body to have a radial projection,
11 against which an insulating body, in particular an
12 insulating material nozzle, is pressed axially by means of a
13 pressure element.

14
15 The radial projection represents a fixed stop for the
16 insulating body. The position of the insulating body with
17 respect to the hollow-cylindrical basic body is thus clearly
18 fixed. The incorporation of the insulating body takes place
19 by means of a pressure element over a short period of time.
20 Additional measurements, adaptations or adjustments of the
21 insulating body are thus not required. An annular disk,
22 which transfers the contact-pressure force evenly over the
23 insulating body, can be used, for example, as the pressure
24 element. In this case, it is advantageous if the radial
25 projection is likewise designed to be annular and
26 circumferential.

27
28 Provision may advantageously also be made for the hollow-
29 cylindrical basic body to have a reduced outer diameter at
30 its end facing the switching path and for the radial
31 projection to be arranged on the hollow-cylinder inner
32 casing in the region of the reduced outer diameter.

33
34 With such an arrangement of the radial projection, a
35 sufficient distance is produced between the contact-pressure

1 cheeks of the projection and the pressure element to make
2 advantageous use of the intrinsic elasticity of the
3 insulating body material. Owing to thermal influences,
4 expansions or shrinkages of the insulating material result.
5 It is therefore necessary when using a clamping connection
6 to cover a sufficient insulating body volume. Only in this
7 manner is it possible for sufficient holding force to act on
8 the insulating body in the case of various thermal loads. A
9 clamping region which is too small would not be suitable for
10 permanently applying the required forces. Furthermore, the
11 insulating body can be stopped very close to the front of
12 the hollow-cylindrical basic body. The required physical
13 length for the total construction of fixing the erosion-
14 resistant ring and the insulating material nozzle to the
15 hollow-cylindrical basic body is thus reduced.

16
17 A further advantageous refinement may provide for the ring
18 to have fixing devices in the region of its enlarged radial
19 wall thickness.

20
21 Sections having an enlarged wall thickness make it possible
22 to flexibly select the location of fixing devices. At the
23 same time, such sections have a comparatively high
24 mechanical strength. For example, threaded holes or other
25 anchoring points may be provided as the fixing devices.

26
27 Provision may advantageously be made for contact-making
28 points between the two rated current contact pieces to lie
29 axially in the region of the arc-resistant material in the
30 switched-on state of the switching device.

31
32 An arrangement of the contact-making points of the two rated
33 current contact pieces in the region of the arc-resistant
34 material prevents, from the outset, a situation in which the
35 individual contact faces need to be moved over joints during

1 a switching operation. As a result, the joints are protected
2 against mechanical loading resulting from the corresponding
3 contact parts of the rated current contact pieces being
4 pushed on and pushed away. For this reason it is possible to
5 manufacture the joints with increased tolerance. It is
6 barely possible for an electroplating to be removed at this
7 joint owing to mechanical loading of the rated current
8 contact pieces. The robustness of the contact pieces of the
9 switching device is thus improved.

10
11 The invention will be shown schematically in a drawing and
12 described in more detail below with reference to an
13 exemplary embodiment.

14
15 In the drawing

16
17 Figure 1 shows a section through a switching device,

18
19 Figure 2 shows a further section through the switching
20 device, and

21
22 Figure 3 shows a section through the switching device shown
23 in figures 1 and 2, along the axis A-A.

24
25 The switching device illustrated in figure 1 is a high-
26 voltage power breaker 1. A high-voltage power breaker 1 is
27 used to switch rated currents and short-circuit currents.
28 The high-voltage power breaker 1 has a first arcing contact
29 piece 2 and a second arcing contact piece 3. The first
30 arcing contact piece 2 is essentially cylindrical and has a
31 coating of an arc-resistant material at its end facing the
32 switching path of the high-voltage power breaker 1. The
33 second arcing contact piece 3 is in the form of a tulip
34 contact, in which the first arcing contact piece 2 can be
35 inserted. At its end facing the switching path, the second

1 arcing contact piece 3 likewise has a coating of arc-
2 resistant material. The two arcing contact pieces 2, 3 are
3 arranged axially opposite one another on a main axis 4. A
4 first rated current contact piece 5 is arranged
5 concentrically with respect to the first arcing contact
6 piece 2. A second rated current contact piece 6 is arranged
7 concentrically with respect to the second arcing contact
8 piece 3. The first rated current contact piece 5 has a large
9 number of elastic contact fingers 7 at its end facing the
10 switching path, said contact fingers 7 being in electrically
11 conductive contact with the outer casing of the second rated
12 current contact piece 6 in the closed state of the high-
13 voltage power breaker 1. Furthermore, the second arcing
14 contact piece 3 is surrounded by an insulating material
15 nozzle 8. The insulating material nozzle 8 is held on the
16 second rated current contact piece 6. The rated current
17 contact pieces 5, 6 and the arcing contact pieces 2, 3 can
18 be moved in relation to one another along the main axis 4,
19 to be precise such that, in the case of a switch-on
20 operation, initially the arcing contact pieces 2, 3 and then
21 the rated current contact pieces 5, 6 come into contact with
22 one another. In the event of a switch-off operation,
23 initially the rated current contacts 5, 6 open, and then the
24 arcing contact pieces 2, 3 are isolated from one another.
25 The second rated current contact piece 6 has an essentially
26 hollow-cylindrical basic body 6a. The hollow-cylindrical
27 basic body 6a is covered at the front by a ring 9 of an arc-
28 resistant material. The ring likewise has an essentially
29 hollow-cylindrical structure, the hollow cylinder top face,
30 which faces the switching path of the high-voltage power
31 breaker 1, being rounded off. Furthermore, the wall
32 thickness of the ring 9 on the side facing away from the
33 switching path is less than on its side facing the switching
34 path. In the present exemplary embodiment, this is achieved
35 by the inner diameter of the ring 9 being enlarged on its

1 side facing away from the switching path. Furthermore, a
2 conical or parabolic profile of the inner casing surface of
3 the ring 9 or other suitable geometric shapes can also be
4 used. The hollow-cylindrical basic body 6a has a reduced
5 outer diameter at its end facing the switching path. The
6 reduced outer diameter of the hollow-cylindrical basic
7 body 6a and the enlarged inner diameter of the ring 9 are
8 matched to one another such that the ring 9 can be pushed
9 onto the hollow-cylindrical basic body 6a. In order to press
10 the ring 9 against the hollow-cylindrical basic body 6a, the
11 ring 9 has a plurality of threaded holes, into which bolts
12 10 can be screwed. The bolts 10 are supported in each case
13 at edges of cutouts, which are arranged distributed
14 symmetrically, parallel to the main axis 4, in the casing of
15 the hollow-cylindrical basic body 6a. The surface of the
16 ring 9 is electroplated. This electroplating is, for
17 example, a silver plating. The hollow-cylindrical basic
18 body 6a is likewise provided with an electroplating. In the
19 switched-on state of the high-voltage power breaker 1, the
20 contact points of the electrical contact fingers 7 rest in
21 the region 11 of the ring 9. Owing to the arrangement of the
22 ring 9 of an arc-resistant material, high switching powers
23 can also be controlled, in the case of which switching arcs
24 occur, despite the use of arcing contact pieces, even on the
25 rated current contact pieces. The use of the arc-resistant
26 ring 9 allows for a compact design of a high-voltage power
27 breaker.

28
29 Figure 2 illustrates a section through the high-voltage
30 power breaker 1 known from figure 1. However, the sectional
31 plane is pivoted about the main axis 4 such that it is now
32 possible to see the fixing of the insulating material nozzle
33 8. The insulating material nozzle 8 is held by means of
34 further bolts 11, which can be screwed into threaded holes
35 in the essentially hollow-cylindrical basic body 6a. In this

1 case, the threaded holes are aligned such that the further
2 bolts 11, just like the bolts 10, are arranged parallel to
3 the main axis 4. The hollow-cylindrical basic body 6a has an
4 annular projection 12. A circumferential shoulder of the
5 insulating material nozzle 8 is pressed against the annular
6 projection 12. The contact-pressure force of the shoulder
7 against the annular projection 12 is produced by means of a
8 pressure element 13 in the form of a pressure disk, which is
9 held by the further bolts 11. The annular projection 12 is
10 arranged on the inner casing side of the essentially hollow-
11 cylindrical basic body 6a, to be precise in the section 14
12 in which the outer diameter of the hollow-cylindrical basic
13 body 6a is reduced.

14
15 Figure 3 shows a section along the sectional plane A-A
16 illustrated in figures 1 and 2. The pressure element 13 has
17 a structure which is in the form of an annular disk and
18 which has cutouts, through which the further bolts 11 pass.
19 The pressure element 13 is pressed against the projection 12
20 by means of the further bolts 11, with the interposition of
21 the projecting shoulder of the insulating material nozzle 8.
22 Furthermore, the pressure element 13 is designed such that,
23 in order to achieve a small total diameter for the
24 arrangement, the pressure element 13 has lateral notches in
25 order to make it possible to fix the ring 9 by means of the
26 bolts 10. This design makes it possible to fix the ring 9 or
27 the insulating material nozzle 8 independently of one
28 another. As a result, the two connections are decoupled from
29 one another. Any interference or thermal expansions etc. at
30 one connection point are thus largely kept away from the
31 other connection.

32
33